

# Optimisation of coagulation process with SIWW is coagulant for colour and COD removal of acid dye effluent using central composite design experiment

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**Abstract:** Central composite rotatable design experiment is used to study the effect of coagulation process for acid dye effluents and to optimise the variables such as dye concentration, coagulant dosage and initial pH, which influence the efficiency of colour and COD removal of dye effluents. The steel industrial wastewater (SIWW) FeCl<sub>3</sub> rich is used for this study as an original coagulant to remove the acid red 14 dye solutions. A model has been obtained among decolourization, COD reduction and relevant parameters by means of variance analysis and obtained model was optimized. The efficiencies of decolourization and COD reduction for acid dye solution were accomplished at optimum conditions as 98% and 94%, respectively.

**Keywords:** Optimization, Coagulation, SIWW, Dye Removal, Acid Red 14, Statistical Design Method

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## 1. Introduction

Dyes are the one of the major constituents of the wastewater produced from many industries related to textile, paint and varnishes, ink, plastics, pulp and paper, cosmetics, tannery etc., and also to the industries, which produces dyes [1].

Colour is one of the most important hazards in industrial effluents, which needs to be treated [2-7], because the presence of dyes in water reduces light penetration, precluding the photosynthesis of aqueous flora [8]. Besides that, some dyes may cause allergy, dermatitis, skin irritation, and cancer to humans [9] in addition to being mutagenic [10].

Treatment of the textile dye containing effluent is difficult and ineffective with conventional biological processes [11] because many synthetic dyes are very stable to light, temperature and resistant to microbial attack.

Considerable efforts have been made by many researchers to find appropriate treatment systems in order to remove pollutants and impurities of wastewaters emanated from different industries, in particular, textile industry [12-16]. Many chemical and physical methods of dye-removal have

been used, including photocatalytic degradation [17], membrane processes [18], adsorption techniques [19], chemical oxidation [20] and coagulation-flocculation [21].

Coagulation-flocculation followed by sedimentation and filtration is used worldwide in the wastewater treatment process before discharge of the treated water to the river. Many coagulants are widely used in the conventional wastewater treatment processes [22]. These coagulants can be inorganic coagulants (e.g., aluminium sulphate, ferric chloride and polyaluminium chloride), synthetic organic polymers (e.g., polyacrylamide derivatives) or naturally occurring flocculants (e.g., microbial flocculants). These coagulants and flocculants are used for different purposes depending on their chemical characteristics [23].

The aim of the present work is to test the ability of the steel industrial wastewater (SIWW) as an original coagulant to remove the acid dye solution. The experiments were planned by using statistical design method [24]. The dye concentration, coagulant dosage and initial pH are chosen as process parameters. The regression models obtained were used in a constrained optimization to find optimum process conditions for maximum decolourization and COD reduction efficiency

of the acid red 14 effluents.

## 2. Materials and Methods

### 2.1. Materials

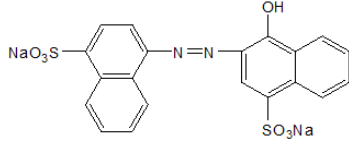


Figure 1. Molecular structure of acid red 14

The acid red 14 was purchased from Aldrich  $C_0$  with a molecular structure as given in Fig. 1. The characteristics of acid dye are summarized in Table 1.

Table 1. The characteristics of acid red 14

Parameter	Value
Colour index number	14720
Chromophore	Monoazo
Chromotrope	FB
Molecular Weight (g/mol)	501.99
$\lambda_{max}$ (nm)	515
Chemical Formula	$C_{20}H_{12}N_2Na_2O_7S_2$

The SIWW was taken from Magreb Steel (Morocco society) and was used as a novel coagulant in this study [25]. The characteristics of SIWW are given in Table 2. Analysis of SIWW sampled at end pipe of this plant indicates a high level of  $FeCl_3$ . Then this rejection was valorised as coagulant in the treatment of textile wastewater .

The decolourization and COD reduction of dye solutions were examined under coagulation processes by jar-test experiment [26].

Table 2. The characteristics of SIWW

Parameter	Value
$FeCl_3$ (mg/L)	1787
Conductivity (ms/cm)	26200
pH value	< 1

### 2.2. Analytical Procedure

The standard stock solution of 1000 mg/L including acid dye was prepared in distilled water. The standard working solutions were prepared by further dilution of standard stock solutions. The solutions were prepared for calibration curves by further dilution of standard working solutions. The initial pH of standard working solutions was adjusted by addition of NaOH or  $H_2SO_4$  to a desired value in the range of 2–6. Samples of dye solutions were measured using a UV/Visible spectrophotometer (Model 7800 UV/VIS) at the beginning and at the end of the experiment. COD removal was detected by using standard methods at the beginning and at the end of the experiment [27]. The percentage of decolourization and COD reduction were calculated as follows. Eq. (1):

$$\text{Decolourization\%/COD reduction\%} = (1 - C/C_0) \times 100 \quad (1)$$

where  $C_0$  is initial dye concentration/COD, C is final dye concentration/COD after treatment by coagulation with SIWW.

### 2.3. Statistical Design of Experiments

The rotatable central composite design  $2^3$  was applied to study the effect of three design factors, namely initial pH of acid dye solutions ( $X_1$ ), coagulant dosage ( $X_2$ ) and dye concentration ( $X_3$ ). The coded levels and the natural values of these factors set in the statistical experiment are shown in Table 3. The design consisted of 16 trials as calculated by the following equation (2):

$$N = 2^k + 2 \times k + n_c = 2^3 + 2 \times 3 + 2 = 16 \quad (2)$$

where N is the total number of runs, k the number of factors, and  $n_c$  is the number of central points. The distance of the axial points from the centre of the rotatable central composite design (star distance,  $\alpha$ ) was calculated [28] by the equation (3):

$$\alpha = 2^{k/4} = 2^{3/4} = 1.682 \quad (3)$$

The selected optimization parameters or responses are the following:  $Y_{DEC}$ , decolourization efficiency (%) and  $Y_{COD}$ , COD reduction (%). The results of the statistical experiment were treated by the software STATGRAPHICS-Plus (Version 4) to determine the various components of analysis of variance (ANOVA).

Table 3. Study field and coded factors

Natural variables ( $x_j$ )	Unit	Coded variables $X_1, X_2, X_3$ *				
		- $\alpha$	1	-1	+ $\alpha$	0
$x_1$ = Initial pH	-	2.32	3	4	5	5.68
$x_2$ = Coagulant dosage	mL	0.16	0.5	1	1.5	1.84
$x_3$ = Dye concentration	mg/L	65.91	100	150	200	234.09

\* The coded values  $X_j = \pm 1$  are obtained by the equation:  $X_j = (x_j - R_j)/\Delta$

## 3. Results and Discussion

### 3.1. Development of Regression Model Equation

The corresponding quadratic models for the above optimization parameters were first computed, from which the outliers (statistically unacceptable measurements) were found and excluded from the subsequent calculations. The insignificant effects (factors and interactions) having p-values higher than 0.05 were then excluded, and those with p-values lower than 0.05 were further used being statistically different from zero at the 95% confidence level.

The experimental design matrix and the corresponding experimental parameters and response value were shown in Table 4. STATGRAPHICS-Plus computer software was used to model and optimize the experimental results. At the end of coagulation processes with SIWW, the final empirical models in terms of coded factors after excluding the insignificant terms for decolourization efficiency ( $\hat{Y}_{DEC}$ ) and COD reduction ( $\hat{Y}_{COD}$ ) of acid dye solutions are shown in Eq. (4)

and Eq. (5), respectively.

$$\hat{Y}_{DEC} = 95.44 + 0.98X_1 + 11.32X_2 - 6.96X_3 - 11.86X_2^2 - 3.38X_3^2 \quad (4)$$

$$\hat{Y}_{COD} = 91.35 + 1.23X_1 + 12.16X_2 - 8.16X_3 - 13.6X_2^2 - 3.17X_3^2 \quad (5)$$

**Table 4.** Experimental design and results for dye removal

Order	Coded units of variable				Responses*		
	Logical	actual	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	Y <sub>DEC exp.</sub>	Y <sub>COD exp.</sub>
1		10	1	1	1	86	79
2		12	1	1	-1	98	98
3		16	1	-1	1	63	58
4		6	1	-1	-1	78	73
5		2	-1	1	1	86	77
6		5	-1	1	-1	97	95
7		9	-1	-1	1	61	56
8		4	-1	-1	-1	76	70
9		7	1.68179	0	0	98	94
10		15	-1.68179	0	0	93	90
11		13	0	1.68179	0	81	74
12		8	0	-1.68179	0	42	30
13		1	0	0	1.68179	73	68
14		11	0	0	-1.68179	98	95
15		14	0	0	0	96	91
16		3	0	0	0	95	92

\* Decolourization efficiency (Y<sub>DEC</sub>) and COD reduction (Y<sub>COD</sub>) of acid red 14.

Positive sign in front of the terms indicates synergistic effect, whereas negative sign indicates antagonistic effect. The quality of the model developed was evaluated based on the correlation coefficient value. The R value for Eq. (4) and Eq. (5) was 0.9977 and 0.9959, respectively. Both the R values obtained were relatively high, indicating that there was a good agreement between the experimental and the predicted values from the models.

The R<sup>2</sup> value for Eq. (4) was 0.9954 and 0.9918 for Eq. (5). This indicated that 99.54 % and 99.18 % of the total variation in the decolourization efficiency and COD reduction of acid red 14 effluents, respectively, was attributed to the experimental variables studied. From the statistical results obtained, it was shown that the above models were adequate to predict the decolourization efficiency and COD reduction of acid dye solutions by coagulation processes with SIWW within the range of variables studied.

**3.2. Decolourization Efficiency of Acid Red 14 Effluents**

The adequacy of the models was further justified through analysis of variance. The ANOVA for the model for decolourization efficiency of acid dye solutions by coagulation processes with SIWW is listed in Table 5.

From this ANOVA, the Model F-value of 360.84 implied that the model was significant. Values of Prob. > F less than 0.05 indicated that the model terms were significant. In this case, initial pH of acid dye solutions (X<sub>1</sub>), coagulant dosage (X<sub>2</sub>), dye concentration (X<sub>3</sub>) and the interaction terms (X<sub>2</sub><sup>2</sup> and X<sub>3</sub><sup>2</sup>), were significant model terms whereas the interaction

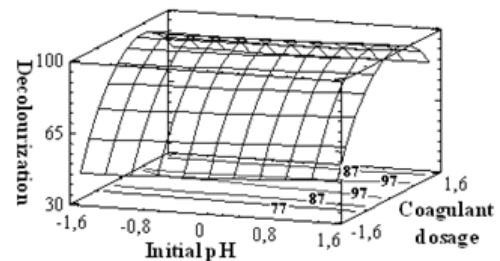
terms (X<sub>1</sub><sup>2</sup>, X<sub>1</sub>X<sub>2</sub>, X<sub>1</sub>X<sub>3</sub> and X<sub>2</sub>X<sub>3</sub>) were insignificant to the response.

**Table 5.** Analysis of variance for decolourization efficiency of acid dye solution

Source of variation	Sum of Squares	Degree of freedom	Mean square	F <sub>exp</sub>	Significance test
Regression	4034,486	9	448.2763	360.84	***
β <sub>1</sub>	13,1656	1	13.1656	10.60	**
β <sub>2</sub>	1749,89	1	1749.89	1408.58	***
β <sub>3</sub>	661,464	1	661.464	532.45	***
β <sub>11</sub>	0,233409	1	0.233409	0.19	NS
β <sub>12</sub>	1,125	1	1.125	0.91	NS
β <sub>13</sub>	0,125	1	0.125	0.10	NS
β <sub>22</sub>	1303,55	1	1303.55	1049.29	***
β <sub>23</sub>	6,125	1	6.125	4.93	NS
β <sub>33</sub>	105,638	1	105.638	85.03	***
Residue	7.45388	6	1.24231	-	-

\*\*\*: Prob. ≤ 0.01, \*\*: Prob. ≤ 0.025, NS: No significant.

A geometrical representation for the decolourization efficiency of acid red 14 effluents by coagulation processes with SIWW, which is dependent on the coagulant dosage and initial pH of acid dye solutions, for constant values of the dye concentration (X<sub>3</sub> = 0), is indicated on Fig. 2. As can be seen from Fig. 2, when the coagulant dosage (X<sub>2</sub> = -α to 0) increase and the initial pH of acid dye solutions increase together or remaining unchanged, then the decolourization efficiency of acid red 14 effluents increase up to 97%.



**Figure 2.** Response surface plot showing the effect of coagulant dosage and initial pH of dye solution on acid dye solution decolourization at fixed dye concentration (150mg/mL)

**3.3. COD Reduction of Acid Red 14 Effluents**

For COD reduction of acid red 14 effluents by coagulation processes with SIWW, the ANOVA for this response is listed in Table 6.

From this ANOVA, the Model F-value of 30.01 implied that the model was significant as well. In this case, the linear terms (X<sub>1</sub>, X<sub>2</sub> and X<sub>3</sub>) and the interaction terms (X<sub>1</sub><sup>2</sup>, X<sub>2</sub><sup>2</sup>, X<sub>3</sub><sup>2</sup> and X<sub>1</sub>X<sub>2</sub>) were significant model terms whereas the interaction terms (X<sub>1</sub>X<sub>3</sub> and X<sub>2</sub>X<sub>3</sub>) were insignificant to the response.

Fig. 3 shows the three-dimensional response surfaces which was constructed to show the effects of the coagulant dosage and the initial pH of acid dye solutions on the COD reduction of acid red 14 effluents by coagulation processes with SIWW. The dye concentration was fixed at zero level. From this geometrical representation, when the coagulant dosage (X<sub>2</sub> = -α to 0) increase and the initial pH of acid dye solutions

remaining unchanged, then the COD reduction of acid red 14 effluents increase up to 93%.

Table 6. Analysis of variance for COD reduction of acid dye solution

Source of variation	Sum of Squares	Degree of freedom	Mean square	F <sub>exp</sub>	Significance test
Regression	11081.23	9	1231.25	30.01	***
$\beta_1$	1847.96	1	1847.96	45.04	***
$\beta_2$	5655.20	1	5655.20	137.84	***
$\beta_3$	396.056	1	396.056	9.65	**
$\beta_{11}$	528.291	1	528.291	12.88	**
$\beta_{12}$	312.5	1	312.5	7.62	*
$\beta_{13}$	18.0	1	18.0	0.44	NS
$\beta_{22}$	2435.36	1	2435.36	59.36	***
$\beta_{23}$	18.0	1	18.0	0.44	NS
$\beta_{33}$	1489.05	1	1489.05	36.29	***
Residue	246.172	6	41.0287	-	-

\*\*\*: Prob.  $\leq 0.01$ , \*\*: Prob.  $\leq 0.025$ , \*: Prob.  $\leq 0.05$ , NS: No significant.

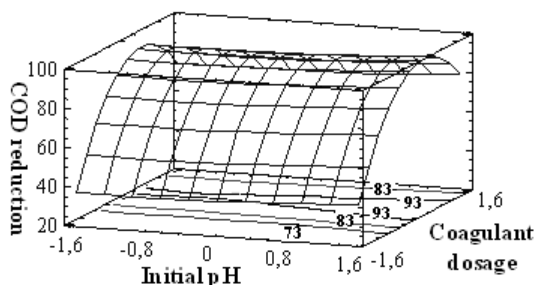


Figure 3. Response surface plot showing the effect of coagulant dosage and initial pH of dye solution on acid dye solution COD reduction at fixed dye concentration (150mg/mL)

### 3.4. Process Optimization

The main objective of this research is to determine the experimental conditions required to remove dye colour and COD. Then, using above mentioned methodology for experimental design, the ranges of the parameters required to obtain optimum conditions were determined. In this optimization study, decolourization efficiency and COD reduction of the acid red 14 effluents were chosen as the objective function. Furthermore, optimum conditions are often calculated in the presence of some constraints which ensure them to be more realistic. If the model used in the optimization study is an empirical one, high and low levels of the process parameters in the experimental design are considered, inevitably, as explicit constraints, in order to avoid extrapolation. Thus, the optimization problem is defined both responses as [29];

- Maximize;

$$\hat{Y}_{DEC} / \hat{Y}_{COD} \quad (6)$$

- Constraints on the parameters X;

$$-\alpha_i < X_i < +\alpha_i \quad i = 1, 2, 3 \quad (7)$$

The investigation of equations 4 and 5 showed that, if X1 = 1.25, X2 = 0 and X3 = 0; the value predict of decolourization efficiency and COD reduction are 96.67% and 92.89%, respectively. The experimental checking in this point, i.e.

under the conditions such as: initial pH of acid dye solution = 5.25, coagulant dosage = 1 mL and dye concentration = 150 mg/L with Y<sub>DEC</sub> = 98% and Y<sub>COD</sub> = 94%, confirms this results.

## 4. Conclusion

The present study clearly demonstrated the applicability of SIWW is very effective coagulant for dye removal. This study showed that response surface methodology was one of the suitable methods to optimize the best operating conditions to maximize the dye removal. Graphical response surface was used to locate the optimum point. A central composite rotatable design was successfully employed for experimental design and analysis of results.

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