

# Fiber Fuse Simulation in Dispersion-Shifted Fibers

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**Abstract:** Silica-based optical fibers are the most important transmission medium for long-distance and large-capacity optical communication systems. The most distinguished feature of optical fiber is its low loss characteristics. A single-mode optical fiber (SMF) exhibits a very low transmission loss (0.142 dB/km) at 1.55  $\mu\text{m}$ . Together with such low loss characteristics, zero chromatic dispersion near 1.55  $\mu\text{m}$  is required for high capacity signal transmission. The zero-dispersion wavelength of optical fibers can be shifted to the vicinity of 1.55  $\mu\text{m}$  by the mutual cancellation of material dispersion and waveguide dispersion. Such fibers are called dispersion-shifted fibers (DSFs). The unsteady-state thermal conduction process in several DSFs was studied theoretically by the explicit finite-difference method using the thermochemical  $\text{SiO}_x$  production model. The calculated threshold power and velocity of fiber fuse propagation in a step-index SMF were in fair agreement with the experimental values observed at 1.55  $\mu\text{m}$ . It was found that the calculated threshold powers were proportional to the effective cross sectional areas of several DSFs and there is a linear relationship between the threshold powers and the mode-field diameters in the range of up to 2 W. These results were in fair agreement with the experimental results observed at 1.55  $\mu\text{m}$ .

**Keywords:** Fiber Fuse Phenomenon, Dispersion-Shifted Fibers, Finite-Difference Technique

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## 1. Introduction

Silica-based optical fibers are the most important transmission medium for long-distance and large-capacity optical communication systems. The most distinguished feature of optical fiber is its low loss characteristics. A very low loss single-mode fiber (SMF) with a minimum loss of 0.20 dB/km at a wavelength ( $\lambda_0$ ) of 1.55  $\mu\text{m}$  was reported in 1979 [1], and the lower transmission loss of 0.154 dB/km at  $\lambda_0 = 1.55 \mu\text{m}$  was achieved in 1986 [2], and the lowest transmission loss of 0.142 dB/km at this wavelength was achieved in 2018 [3].

Together with such low loss characteristics, zero chromatic dispersion near  $\lambda_0 = 1.55 \mu\text{m}$  is required for high capacity signal transmission. Chromatic dispersion in a SMF is the sum of material dispersion and waveguide dispersion. A silica-based SMF exhibits zero material dispersion in the vicinity of 1.3  $\mu\text{m}$  [4, 5]. The waveguide dispersion can be controlled by the proper choice of the waveguide parameters, while the material dispersion is almost independent of these parameters. Therefore, the zero-dispersion wavelength  $\lambda_{\text{cd}}^0$ , at which the chromatic dispersion becomes zero, can also be controlled by changing the core diameter, doping

concentration, and relative refractive-index difference  $\Delta$  [6-12].  $\lambda_{\text{cd}}^0$  of SMFs can be shifted to the vicinity of 1.55  $\mu\text{m}$  by the mutual cancellation of material dispersion and waveguide dispersion [6, 7, 11]. Such fibers are called dispersion-shifted fibers (DSFs).

In this article, the unsteady-state thermal conduction process in dispersion-shifted fibers was investigated theoretically with the explicit finite-difference method using the thermochemical  $\text{SiO}_x$  production model [13].

## 2. Characteristics of Dispersion-Shifted Fibers

The waveguide (and also chromatic) dispersion can be tailored by controlling the core size and shape, which is related with the refractive-index profile in the fiber [6]. The DSFs can be classified as single-clad or multi-clad fibers.

### 2.1. Single-Clad Fibers

The single-clad fiber includes a triangular-shape fiber (TriSF) [14, 15]. The refractive-index profile of the TriSF is shown in Figure 1.

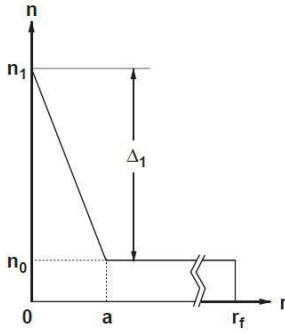


Figure 1. Refractive-index profile of TriSF.

In this figure,  $r_f$  is the fiber radius,  $a$  is the core radius, and  $n_1$  and  $n_0$  are the maximum refractive-index in the core and the cladding refractive-index, respectively.  $\Delta_1$  is the relative refractive-index difference between  $n_1$  and  $n_0$ .

The parameters of two TriSFs are shown in Table 1, together with a conventional step-index SMF.

Table 1. Parameters of step-index SMF and TriSFs.

Parameters	Unit	SMF	TriSF1	TriSF2
$\Delta_1$	%	0.30	0.548	0.80
$a$	$\mu\text{m}$	4.6	2.7	2.7
$\lambda_{\text{cd}}^0$	$\mu\text{m}$	1.31	1.45	1.55
$A_{\text{eff}}$	$\mu\text{m}^2$	93.11	287.52	88.23

In this table,  $A_{\text{eff}}$  is the effective cross sectional area at 1.55  $\mu\text{m}$ , which was estimated with the finite element method (FEM) [16].

Chromatic dispersion in the 1.0-1.7- $\mu\text{m}$  spectral region for the step-index SMF and the TriSFs were calculated by using the FEM program. The calculated results are shown in Figure 2.

It is clear that zero chromatic dispersion of TriSF1 and TriSF2 occurs at 1.45 and 1.55  $\mu\text{m}$ , which is longer than the zero-dispersion wavelength  $\lambda_{\text{cd}}^0$  ( $= 1.31 \mu\text{m}$ ) of the SMF.

However, the TriSFs have one serious disadvantage. It is well known that the  $\text{LP}_{11}$  mode cutoff wavelength in them is shorter than 1  $\mu\text{m}$  [14, 15], which is too far from the operating wavelength of 1.55  $\mu\text{m}$ . Accordingly, the spread of the modal field into the cladding is quite large, as shown in the  $A_{\text{eff}}$  value ( $= 287 \mu\text{m}^2$ ) of TriSF1 (see Table 1), and therefore, the TriSFs exhibit excessive sensitivity to bend-induced losses.

The spread of the field in the cladding can be reduced by introducing extra cladding layers around the core. Such multi-clad fiber is described below.

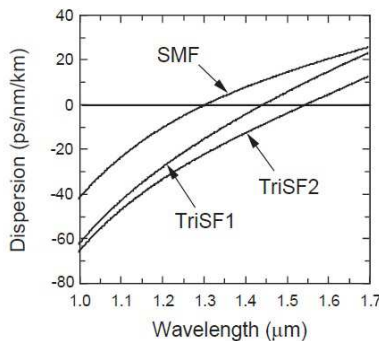


Figure 2. Chromatic dispersion of step-index SMF and TriSFs.

## 2.2. Multi-clad Fibers

The multi-clad fibers include the  $W$ -type fiber with a narrow depressed cladding layer [17-19], the segmented-core fiber [20, 21], and the dual-shape core fiber (DSCF) [22-24]. Among these core/cladding designs, the dual-shape core design has been widely used in the conventional DSF and in the non-zero DSF (NZ-DSF).

As the DSF and NZ-DSF exhibit higher Raman gain efficiencies than those of the step-index SMFs [25, 26], these fibers have been used in long-haul transmission systems employing distributed Raman amplifiers [25, 27-32].

In contrast, a broad dispersion compensation fiber (BDCF) [33, 34] with large negative chromatic dispersion in the 1.55  $\mu\text{m}$  region has also been employed in the Raman amplifiers [35-39].

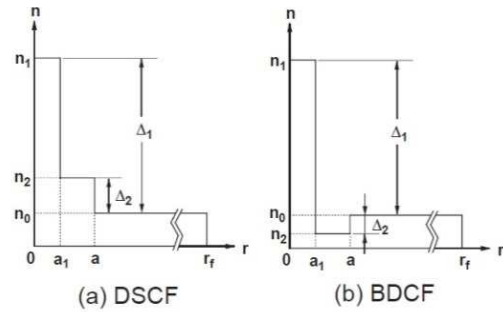


Figure 3. Refractive-index profiles of a DSCF and BDCF.

The refractive-index profile of the DSCF and BDCF are shown in Figure 3.

In this figure,  $a_1$  and  $a$  are the inner and outer core radii, and  $n_1$  and  $n_2$  are the refractive indices in the inner and outer core, respectively.  $\Delta_2$  is the relative refractive-index difference between  $n_2$  and  $n_0$ .

The BDCF is a kind of  $W$ -type fiber with a depressed cladding layer. In this fiber,  $n_2$  is smaller than  $n_0$ , and therefore,  $\Delta_2$  takes a negative value.

The parameters of three types of DSCFs and the BDCF are shown in Table 2.

Table 2. Parameters of DSCFs and BDCF.

Parameters	Unit	NZ(+)-DSF	DSF	NZ(-)-DSF	BDCF
$\Delta_1$	%	0.62	0.74	0.90	1.90
$\Delta_2$	%	0.124	0.148	0.180	-0.35
$a$	$\mu\text{m}$	3.6	3.2	3.0	4.44
$a_1$	$\mu\text{m}$	1.8	1.6	1.5	1.4
$\lambda_{\text{cd}}^0$	$\mu\text{m}$	1.50	1.55	1.61	-
$A_{\text{eff}}$	$\mu\text{m}^2$	79.30	70.25	54.18	16.60

Chromatic dispersions in the 1.3-1.7- $\mu\text{m}$  spectral region for the step-index SMF and the DSCFs are shown in Figure 4.

It is clear that zero chromatic dispersion of the DSF occurs between those of NZ(+)-DSF and NZ(-)-DSF, and the zero-dispersion wavelengths  $\lambda_{\text{cd}}^0$  of these fibers are longer than that of the SMF.

Chromatic dispersions in the 1.3-1.7- $\mu\text{m}$  spectral region for the step-index SMF and the BDCF are shown in Figure 5.

It is clear that the BDCF exhibits large negative chromatic

dispersion (about -110 ps/km·nm) and dispersion slope (about -0.443 ps/km/nm<sup>2</sup>) at 1.55 μm. This fiber can compensate the dispersion and dispersion slope of the conventional step-index SMF over the optical bandwidth of more than 100 nm [35, 37, 40].

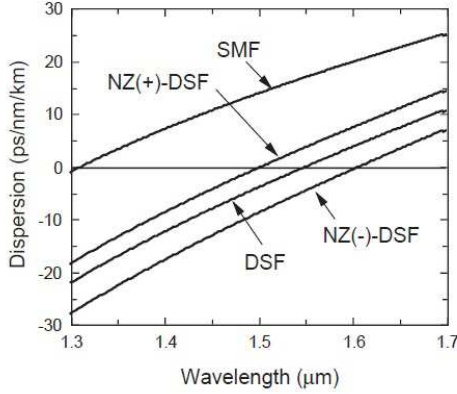


Figure 4. Chromatic dispersion of step-index SMF and DSCFs.

In the next section, the results of some numerical calculations related to the thermal conduction process in various DSFs are described.

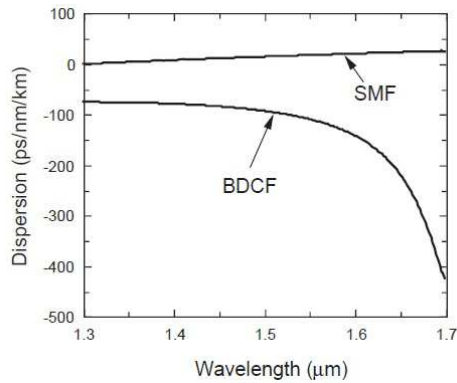


Figure 5. Chromatic dispersion of step-index SMF and BDCF.

### 3. Fiber Fuse Calculation in DSFs

The first fiber fuse experiments were conducted in two TriSFs (TriSF1 and TriSF2 in Table 1) by Kashyap and co-workers, together with a step-index SMF at  $\lambda_0 = 0.514$  and  $1.064$  μm [41-43]. We reported that the propagation velocities of fiber fuse in a step-index SMF and TriSFs, which were theoretically estimated at  $\lambda_0 = 1.064$  μm, were in fairly good agreement with the experimentally determined values [44, 45]. Several experiments had also been carried out on the fiber fuse phenomenon in the DSFs at  $\lambda_0 = 1.064$ ,  $1.467$ , and  $1.55$  μm [46-53].

In this section, we do some numerical calculations related to the thermal conduction process in the DSF at  $\lambda_0 = 1.55$  μm.

We assume that the DSF is in an atmosphere of  $T = T_a$  and  $r_f$  of the DSF is  $62.5$  μm. We also assume that part of the core layer is heated and has a length of  $\Delta L$  ( $= 40$  μm) and a temperature of  $T_c^0$  ( $> T_a$ ) (see Figure 6).

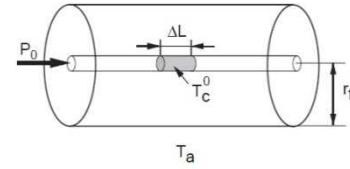


Figure 6. Schematic view of hot zone in core layer.

In the heating zone (called the “hot zone”) shown in Figure 6, an absorption coefficient  $\alpha$  is larger than in the other parts of the core because of its high temperature  $T_c^0$  ( $> T_a$ ). Thus, as the light propagates along the positive direction (away from the light source) in this zone, a considerable amount of heat is produced by light absorption.

The heat conduction equation for the temperature field  $T(r, z, t)$  in the DSF is given by [54]

$$\rho C_p \frac{\partial T}{\partial t} = k \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q} \quad (1)$$

where  $\rho$ ,  $C_p$ , and  $k$  are the density, specific heat, and thermal conductivity of the fiber, respectively.

The last term  $\dot{Q}$  in Eq. (1) represents the heat source caused by light absorption, which is required only for the hot zone in the fiber core.  $\dot{Q}$  can be given by

$$\dot{Q} = \alpha I \quad (2)$$

where  $I$  is the optical power intensity of the core layer.

We assume that the  $I$  value is given by dividing the optical power by the effective cross sectional area of the DSF. That is,  $I$  is given by

$$I = \frac{P_0}{A_{eff}} \quad (3)$$

where  $P_0$  is the incident optical power.

We investigated the core center temperature distribution in the longitudinal direction of the SMF and DSF after the incidence of a laser power  $P_0$  of up to 2 W. The calculation by the finite-difference method followed the procedure described in the literature [13]. In the calculation, the time interval  $\delta t$  was set to 10 ns, the step size along the  $r$  axis  $\delta r$  to  $r_f/14$ , and the step size along the  $z$  axis  $\delta z$  to 20 μm, respectively, and it was assumed that  $T_c^0 = 2,923$  K and  $T_a = 298$  K.

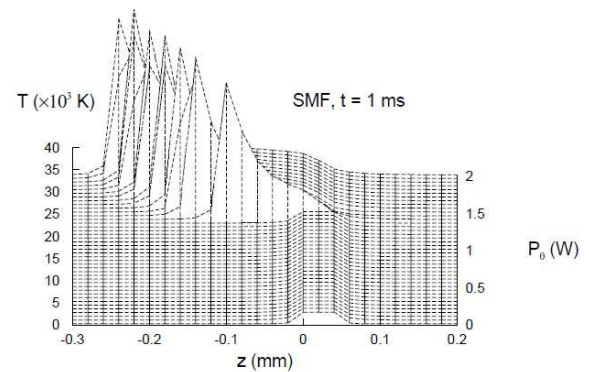
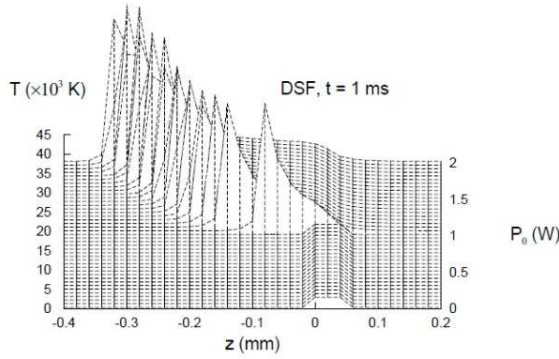


Figure 7. Core center temperature distribution in the longitudinal direction of the SMF after 1 ms when  $P_0 = 0-2$  W and  $\lambda_0 = 1.55$  μm.

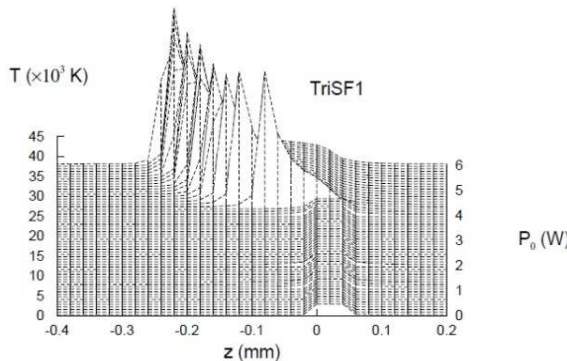
We estimated the change in the temperature  $T(0, z)$  at the core center ( $r = 0 \mu\text{m}$ ) in the SMF and DSF at  $t = 1 \text{ ms}$  after the incidence of laser light with  $\lambda_0 = 1.55 \mu\text{m}$  and initial power  $P_0 = 0\text{--}2 \text{ W}$ . The calculated changes in the temperature at the core center position are shown in Figures 7 and 8.

When the power of the light entering the SMF increases from 1.3 W to 1.4 W, the peak temperature rises from 2,923 to 34,000 K, and thereafter, propagation behavior was observed in the  $-z$  direction with increasing  $P_0$ , as shown in Figure 7. The characteristic  $P_0$  value of 1.4 W is the threshold power  $P_{\text{th}}$  of the SMF. This value is close to the experimental  $P_{\text{th}}$  value of 1.39 W [53]. The  $P_{\text{th}}$  of the DSF is determined as 1.05 W in the same manner as the SMF, as shown in Figure 8.



**Figure 8.** Core center temperature distribution in the longitudinal direction of the DSF after 1 ms when  $P_0 = 0\text{--}2 \text{ W}$  and  $\lambda_0 = 1.55 \mu\text{m}$ .

Furthermore, the change in the temperature  $T(0, z)$  at the core center ( $r = 0 \mu\text{m}$ ) in the TriSF1 was investigated at  $t = 1 \text{ ms}$  after the incidence of a laser power  $P_0$  of up to 6 W. The calculated change in the temperature at the core center position is shown in Figure 9. As shown in this figure, when the power of the light entering the TriSF1 increases from 4.2 W to 4.3 W, the peak temperature rises from 2,923 to 34,000 K, and thereafter propagation behavior was observed in the  $-z$  direction with increasing  $P_0$ . The  $P_{\text{th}}$  of the TriSF1 is determined to 4.28 W. This value is three or four times larger than that of the SMF (1.40 W) or DSF (1.05 W) because the  $A_{\text{eff}}$  value of the TriSF1 is larger than that of the SMF or DSF.

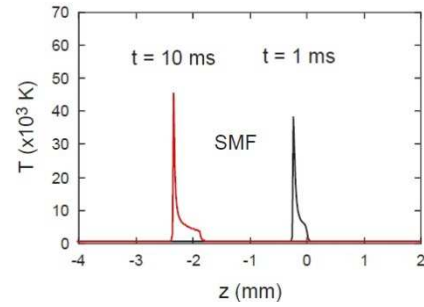


**Figure 9.** Core center temperature distribution in the longitudinal direction of the TriSF1 after 1 ms when  $P_0 = 0\text{--}6 \text{ W}$  and  $\lambda_0 = 1.55 \mu\text{m}$ .

Next, the temperature field of the core center of the SMF was estimated along the  $z$  direction at  $t = 1 \text{ ms}$  and 10 ms

after the incidence of laser light with  $P_0 = 2 \text{ W}$  and  $\lambda_0 = 1.55 \mu\text{m}$ .

The calculated results are shown in Figure 10.



**Figure 10.** Temperature fields of the core center of SMF after 1 and 10 ms when  $P_0 = 2 \text{ W}$  and  $\lambda_0 = 1.55 \mu\text{m}$ .

As shown in Figure 10, the core center temperature near the end of the hot zone ( $z = -0.24 \text{ mm}$ ) changes abruptly to a high value of about  $3.5 \times 10^4 \text{ K}$  after 1 ms. This rapid rise in the temperature initiates the fiber fuse propagation. After 10 ms, the high-temperature front in the core layer reaches a  $z$  value of  $-2.62 \text{ mm}$ . The average propagation velocity  $V_f$  is estimated to be 0.26 m/s using these data. This  $V_f$  is close to the value ( $\sim 0.32 \text{ m/s}$ ) measured by Abedin and Nakazawa [53].

The parameters and  $P_{\text{th}}$  values of various fibers are shown in Table 3.

**Table 3.** Parameters and  $P_{\text{th}}$  values of various fibers.

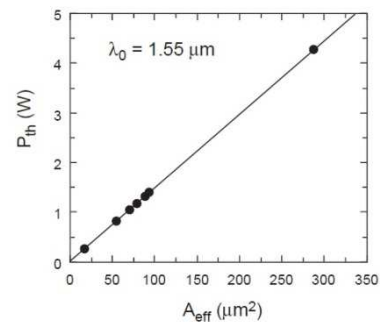
Fibers	$A_{\text{eff}} (\mu\text{m}^2)$	$\omega (\mu\text{m})$	$P_{\text{th}} (\text{W})$
SMF	93.11	5.60	1.40
TriSF1	287.52	9.85	4.28
TriSF2	88.23	5.45	1.32
NZ(+)-DSF	79.30	5.17	1.19
DSF	70.25	4.87	1.05
NZ(-)-DSF	54.18	4.27	0.82
BDCF	16.60	2.37	0.26

In this table,  $\omega$  is the mode field radius at  $\lambda_0 = 1.55 \mu\text{m}$ .  $\omega$  is approximately defined as

$$\omega = \sqrt{\frac{A_{\text{eff}}}{k\pi}} \quad (4)$$

where  $k$  ( $= 0.944$ ) is the correction factor of  $A_{\text{eff}}$  and  $\omega$  [55].

We examined the  $A_{\text{eff}}$  dependence of the  $P_{\text{th}}$  values at  $\lambda_0 = 1.55 \mu\text{m}$ . The results are shown in Figure 11.



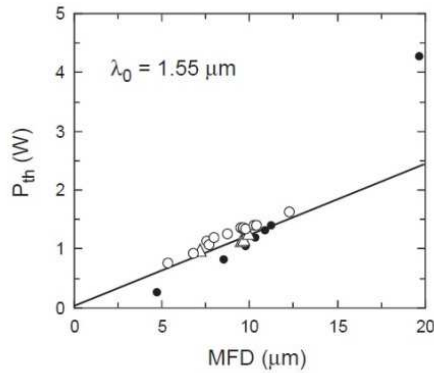
**Figure 11.** Effective cross-sectional area dependence of the threshold powers at  $\lambda_0 = 1.55 \mu\text{m}$ .



As shown in Figure 11, the  $P_{th}$  values are proportional to the  $A_{eff}$  values.

On the other hand, several researchers reported that the  $P_{th}$  value is linearly proportional to the mode-field diameter MFD ( $= 2\omega$ ) at  $\lambda_0 = 1.55 \mu\text{m}$  [51, 52].

Figure 12 shows the MFD dependence of the  $P_{th}$  value of various fibers.



**Figure 12.** MFD dependence of the threshold powers at  $\lambda_0 = 1.55 \mu\text{m}$ . The closed circles are the calculated values, the open circles are the data reported by Takenaga et al. [51], and the open triangles are the data reported by Takara et al. [52].

It was found that there is a linear relationship between the  $P_{th}$  values and MFD value in the range of  $P_{th} < 2 \text{ W}$ . This result is the same as that observed by Takenaga et al. [51] and Takara et al. [52], as shown in Figure 12.

From these results, it can be concluded that expanding the MFD and increasing the  $A_{eff}$  is an effective way to raise the power threshold for fiber fuse propagation in the dispersion-shifted fibers.

## 4. Conclusion

Together with such low loss characteristics, zero chromatic dispersion near  $1.55 \mu\text{m}$  is required for high capacity signal transmission. The zero-dispersion wavelength of optical fibers can be shifted to the vicinity of  $1.55 \mu\text{m}$  by the mutual cancellation of material dispersion and waveguide dispersion. Such fibers are called dispersion-shifted fibers (DSFs). The unsteady-state thermal conduction process in several DSFs was studied theoretically by the explicit finite-difference method using the thermochemical  $\text{SiO}_x$  production model. The calculated threshold power and velocity of fiber fuse propagation in a step-index SMF were in fair agreement with the experimental values observed at  $1.55 \mu\text{m}$ . It was found that the calculated threshold powers were proportional to the effective cross sectional areas of several DSFs and there is a linear relationship between the threshold powers and the mode-field diameters in the range of up to  $2 \text{ W}$ . These results were in fair agreement with the experimental results observed at  $1.55 \mu\text{m}$ .

## Acknowledgements

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